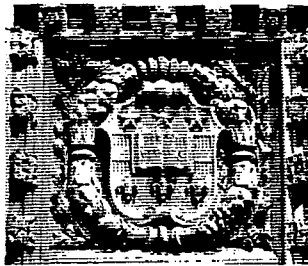


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WASHINGTON UNIVERSITY

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MAPPING SATELLITE-BORNE NARROW-BEAM ANTENNA
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A COMPUTER PROGRAM FOR MAPPING SATELLITE-BORNE NARROW-BEAM ANTENNA FOOTPRINTS ON EARTH

Thomas W. Stagl
Jai P. Singh



PROGRAM ON APPLICATION OF COMMUNICATIONS SATELLITES
TO EDUCATIONAL DEVELOPMENT

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- 1 -

A COMPUTER PROGRAM FOR MAPPING SATELLITE-BORNE
NARROW-BEAM ANTENNA FOOTPRINTS ON EARTH

I. INTRODUCTION

A computer program has been developed that computes the locus of intersection of a quadric cone and a sphere. The outputs of the program are a list of the longitude and latitude coordinates of the locus of intersection and a plot of the locus. It was written primarily to define the area of the earth covered by a narrow-beam antenna carried on a synchronous satellite in circular, near equatorial orbits.

The program is basically an implementation of a report by S. L. Zolnay^[1] with some modifications added. The main modifications are the incorporation of an elliptical cross section antenna beam and computation of the beam vertex angles and corresponding locus of intersection for any signal level between 0.1 and 10 db down from the beam center. Any number of signals up to 10 may be input for each data set. The output will be plotted on the same graph.

The program was written for use with a Cal Comp 570/563 off-line plotting system and uses the standard Cal Comp subroutines supplied with the system. The plot is drawn using linear longitude and latitude scales and non-linear scales such as Mercator scales cannot be used.

It should be noted that this program assumes the earth to be spherical rather than oblate as it actually is. However, by assuming a spherical earth, one introduces maximum error distances of about 11.5 nautical miles. For many purposes, this error can be ignored.

II. MATHEMATICAL ANALYSIS

Figure 1 shows the intersection geometry. The satellite is located at point SAT in a circular, near-equatorial orbit which is a distance DIST from center of the earth. Point P is the point of intersection of satellite antenna boresight (or beam center) and the earth. AL is the arc from the point on earth directly below the satellite (the subsatellite point) to P and is given by:

$$AL = \cos^{-1} [\cos(LONCTR)\cos(LACTR + DELT)] \quad (1)$$

Where LATCTR is latitude of P, LONCTR is the longitude of P relative to the subsatellite point, and DELT is the instantaneous declination angle formed by a vector from satellite to the center of the earth and the equatorial plane. At DIST = ~~39,220~~^{22,300} statute miles (geostationary equatorial orbit when DELT = 0), the maximum arc, AL, permissible for the point to be seen by the satellite is 81.3°. When AL is computed to be larger than 81.3°, the point is over the horizon seen by the satellite and any attempt at finding the locus of intersection would produce meaningless results. Therefore, the computation stops at this point.

The next step is to calculate the vector, RS, extending from the satellite to point P. A right-handed coordinate system is constructed with the origin at SAT, the positive Y axis extending through the earth center and the Z axis in the plane defined by SAT and the north and south poles. The vector RS is given in terms of coordinates along these axes:

$$\begin{aligned} \underline{RS} = & RE \cos(LATCTR) \sin(LONCTR) \underline{i} + \\ & [DIST \cos(DELT) - RE \cos(LATCTR) \cos(LONCTR)] \underline{j} + \\ & [DIST \sin(DELT) + RE \sin(LATCTR)] \underline{k} \end{aligned} \quad (2)$$

Where RE is radius of earth, and i, j and k are unit vectors in the positive x, y, and z directions, respectively.

Pitch and roll angles are then defined as in Figure 2. These are given by:

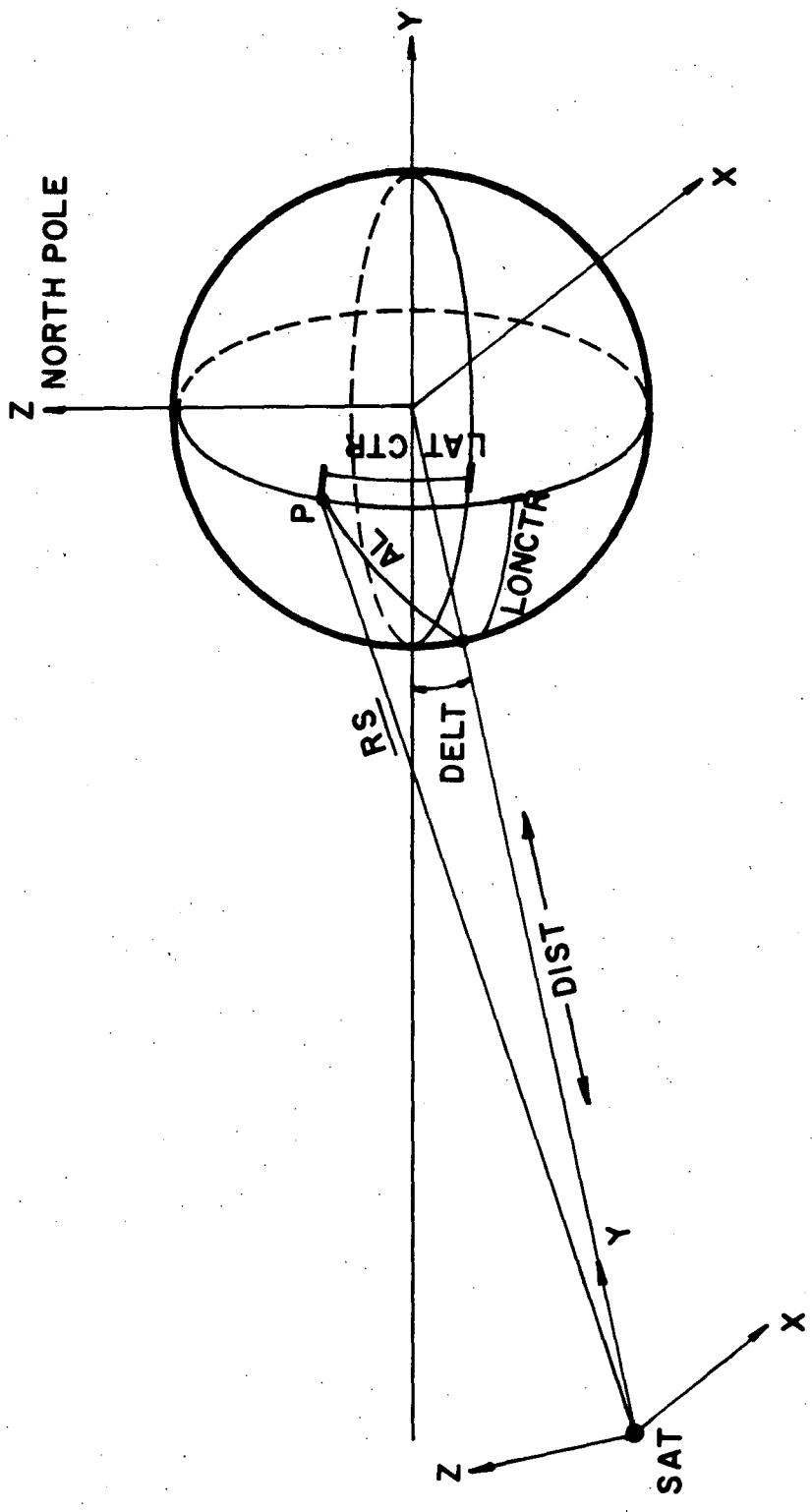


FIGURE 1 GEOMETRY OF INTERSECTION

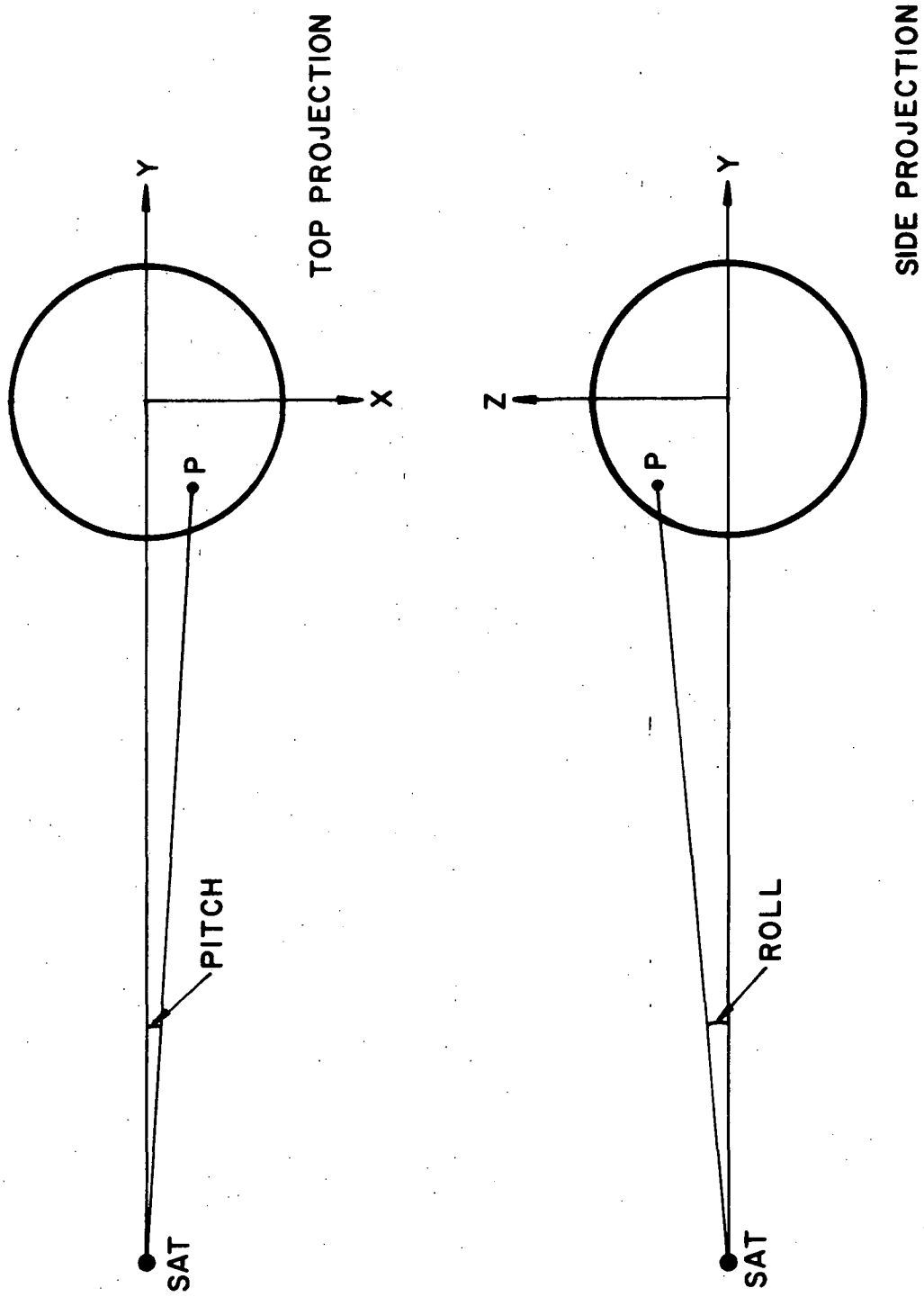


FIGURE 2 GRAPHIC DESCRIPTION OF PITCH AND ROLL ANGLES

$$\text{PITCH} = \sin^{-1} \frac{RS_{\underline{i}}}{\sqrt{RS_{\underline{i}}^2 + RS_{\underline{j}}^2}} \quad (3)$$

$$\text{ROLL} = \tan^{-1} \frac{RS_{\underline{k}}}{\sqrt{RS_{\underline{i}}^2 + RS_{\underline{j}}^2}} \quad (4)$$

A new coordinate system is defined by rotating the old system about its z-axis by an angle equal to PITCH, and then about the resultant x-axis by an angle equal to ROLL.

A vector U is then defined as lying in a plane perpendicular to vector RS. The origin of vector U is at the point of intersection of RS and that plane, see Figure 3.

The equation defining U is:

$$\underline{U} = [\cos(\text{BETA}) \underline{i}' + \sin(\text{BETA}) \underline{k}'] [A^{-2} \cos^2(\text{BETA}) + B^{-2} \sin^2(\text{BETA})]^{-1/2} \quad (5)$$

where i' and k' are unit vectors in the new coordinate system. This equation is a parametric equation of an ellipse with BETA as the parameter and A and B corresponding to the semi-major and semi-minor axes, respectively.

A ray on the surface of the beam can now be generated by a vectorial addition of RS and U. By incrementing BETA from 0° to 360° the entire outer surface of the beam can be generated.

Let a vector Mn be a surface generator vector. The equation defining Mn in the new coordinate system is:

$$\begin{aligned} \underline{Mn} = & [|\underline{RS}| \cos(\text{ROLL}) \sin(\text{PITCH}) + |\underline{U}| \cos(\text{BETA}) \cos(\text{PITCH}) \\ & - |\underline{U}| \sin(\text{BETA}) \sin(\text{ROLL}) \sin(\text{PITCH})] \underline{i}' \\ & + [|\underline{RS}| \cos(\text{ROLL}) \cos(\text{PITCH}) + |\underline{U}| \cos(\text{BETA}) \sin(\text{PITCH}) \\ & - |\underline{U}| \sin(\text{BETA}) \sin(\text{ROLL}) \cos(\text{PITCH})] \underline{j}' \\ & + [|\underline{RS}| \sin(\text{ROLL}) + |\underline{U}| \sin(\text{BETA}) \cos(\text{ROLL})] \underline{k}' \quad (6) \end{aligned}$$

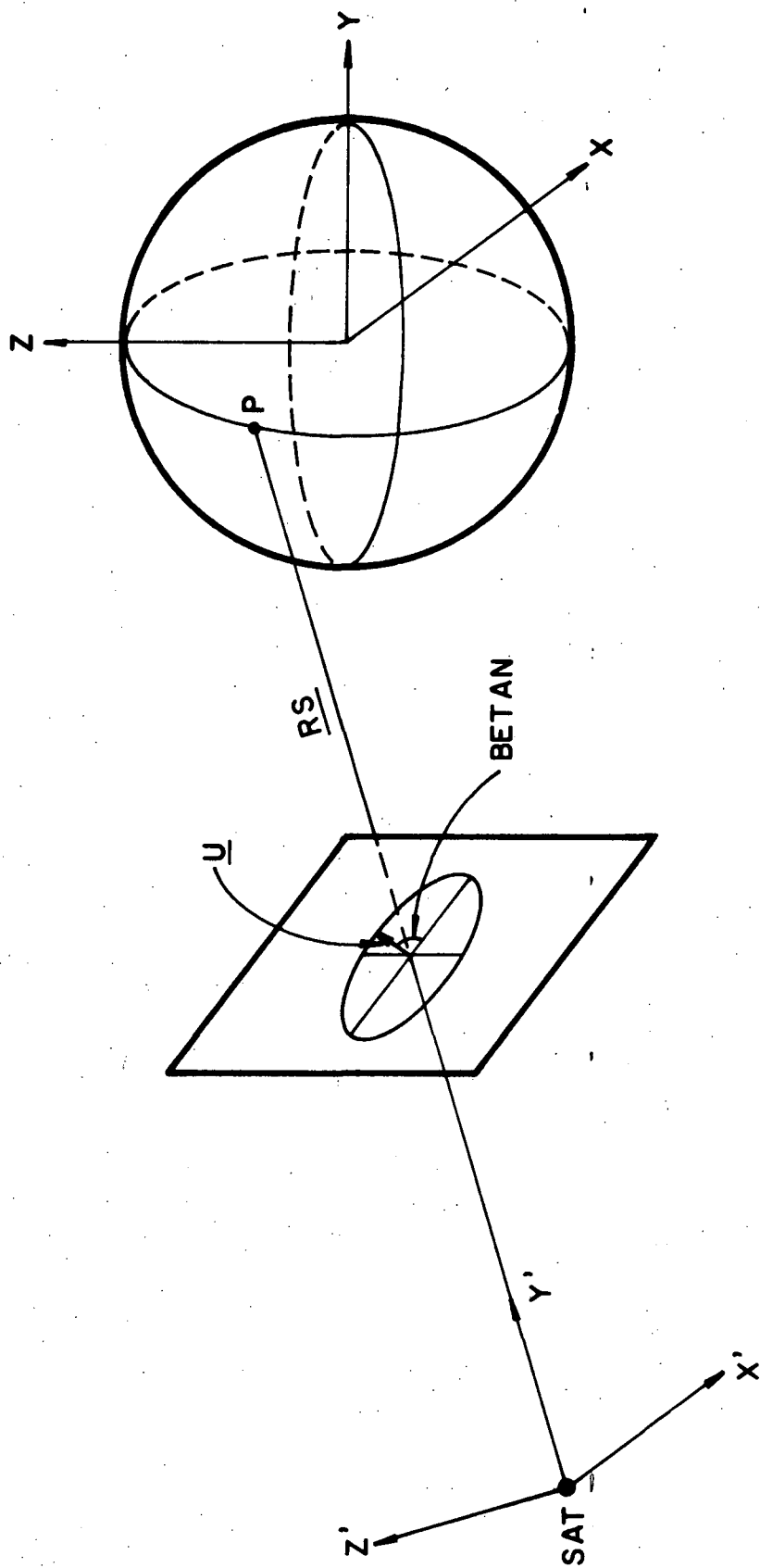


FIGURE 3 GRAGHC DESCRIPTION OF BEAM CROSS SECTION

In the old coordinate system:

$$\begin{aligned} \underline{Mn} = & [Mn_{\underline{i}},] \underline{i} + [Mn_{\underline{j}}, \cos(\text{DELT}) + Mn_{\underline{k}}, \sin(\text{DELT})] \underline{j} \\ & + [-Mn_{\underline{j}}, \sin(\text{DELT}) + Mn_{\underline{k}}, \cos(\text{DELT})] \underline{k} \end{aligned} \quad (7)$$

Pitch and roll angles are defined for each \underline{Mn} as follows:

$$\text{PITCH } N = \text{Sin}^{-1} \frac{Mn_{\underline{i},}}{\sqrt{Mn_{\underline{i},}^2 + Mn_{\underline{j},}^2}} \quad (8)$$

$$\text{ROLL } N = \text{Tan}^{-1} \frac{Mn_{\underline{k},}}{\sqrt{Mn_{\underline{i},}^2 + Mn_{\underline{j},}^2}} \quad (9)$$

The earth radius vector to the point of intersection of \underline{Mn} is:

$$\begin{aligned} \underline{RE} = & [Mn \cos(\text{ROLLN}) \sin(\text{PITCHN})] \underline{I} \\ & + [\text{DIST} \cos(\text{DELT}) - Mn \cos(\text{ROLLN}) \cos(\text{PITCHN})] \underline{J} \\ & + [Mn \sin(\text{ROLLN}) - \text{DIST} \sin(\text{DELT})] \underline{K} \end{aligned} \quad (10)$$

Where Mn is the length of \underline{Mn} and \underline{I} , \underline{J} , and \underline{K} are unit vectors in an earth centered coordinate system whose positive z axis extends through the north pole and positive x axis intersects the 0° meridian.

The latitude and relative longitude coordinates of the point of intersection of \underline{Mn} are found by:

$$\text{LAT} = \text{Tan}^{-1} \frac{RE_{\underline{K}}}{\sqrt{RE_{\underline{I}}^2 + RE_{\underline{J}}^2}} \quad (11)$$

$$\text{LON} = \text{Sin}^{-1} \frac{RE_{\underline{I}}}{\sqrt{RE_{\underline{I}}^2 + RE_{\underline{J}}^2}} \quad (12)$$

The actual longitude is found by adding the above longitude to the longitude of the subsatellite point.

The relative beamwidth for any signal level is found using a beam-width conversion chart. The particular chart used in this program is taken from Microwave Engineers Handbook^[2], (see Figure 4). The actual conversion in the program is done by using linear interpolation between the appropriate two consecutive points from the following set:

(.1, .18) (.2, .26) (.5, .4) (1., .56) (1.5, .7) (3., 1.) (5., 1.27) (10., 1.7)

These points were chosen such that the graph segment between any two consecutive points is approximately linear.

The above discussion assumes that the entire antenna beam intersects the earth. The case when the boresight location is near enough to the horizon that a portion of the beam passes the earth is considered next.

Define an angle, B_n formed by the vector \underline{M}_n and the vector from the satellite to earth center. The angle at which \underline{M}_n is tangent to the earth is given, from the law of sines, as:

$$B_{\max} = \sin^{-1} \frac{RE}{DIST} \quad (13)$$

When the angle B_n is larger than B_{\max} the earth radius vector \underline{RE} must be computed to the point of tangency, i.e. the horizon seen by the satellite. The vector \underline{RE} is then defined by:

$$\begin{aligned} \underline{RE} = & RE [\cos(B_{\max}) \sin(TAUN)] \underline{I} \\ & - RE [\cos(DELT) \sin(B_{\max}) \\ & + \sin(DELT) \cos(B_{\max}) \cos(TAUN)] \underline{J} \\ & - RE [\sin(DELT) \sin(B_{\max}) \\ & - \cos(DELT) \cos(B_{\max}) \cos(TAUN)] \underline{K} \end{aligned} \quad (14)$$

When TAUN is the tilt angle defined by:

$$TAUN = \cos^{-1} \frac{M_{n_k}}{\sqrt{M_{n_i}^2 + M_{n_k}^2}} \quad (15)$$

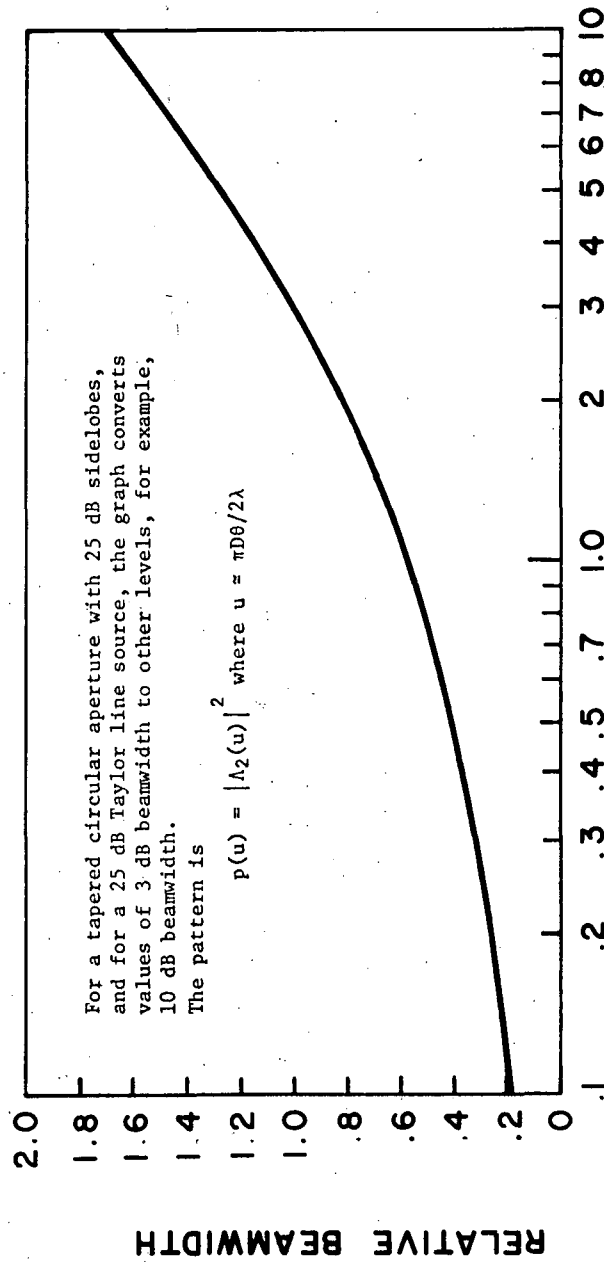


FIGURE 4 BEAMWIDTH CONVERSION

and RE is the radius of the earth. The latitude and relative longitude coordinate are found as in equations (11) and (12).

III. USAGE

The inputs to the program are:

- LONSS - longitude of point on earth directly below satellite (°E)
- LONCT - longitude of boresight intersection (°E)
- LATCT - latitude of boresight intersection (°N)
- INCR - increments of angular parameter BETA, i.e. number of points plotted = $360^\circ/\text{INCR}$
- DELT - instantaneous declination of satellite - earth center vector from plane of equator (°below equatorial plane)
- THETA - orientation angle of elliptical beam about beam center (measured positive counter-clockwise)
- BW1 - beam vertex angle in plane defined by beam vertex and major axis of beam cross section at point 3 db below beam center
- BW2 - beam vertex angle in plane defined by beam vertex and minor axis of beam cross section at point 3 db below beam center
- L - number of signal levels to be plotted
- DB(I) - signal levels to be plotted (measured in db below beam center)

It should be noted that all inputs except L and DB(I) are in degrees rather than radians. Longitude inputs can be expressed as degrees east of 0° or negative degrees west of 0°. The output will agree with the input.

Each input data set will consist of three cards. The format for the data is:

Card #1

column	
1 - 9	LONSS
10 - 18	LONCT
19 - 27	LATCT
28 - 36	INCR
37 - 45	DELT

Card #2

1 - 9	THETA
10 - 18	BW1
19 - 27	BW2
28 - 29	L

Card #3

1 - 7	
8 - 14	DB(I)
15 - 21	

Every input, with the exception of L, must contain a decimal point. The input L must not contain a decimal point and must be right justified in columns 28-29, i.e. single digit input must be in column 29. The inputs DB(I) must be input in increasing order with the signal level closest to beam center listed first and the level farthest from beam center listed last.

The output of the program consists of two parts, the printout and the plot. The printout contains, for each set of input data, a list of the following parameters:

- SUB SAT LONG - longitude of point directly below satellite
- BOR SGHT LONG - longitude of boresight intersection
- BOR SGHT LAT - latitude of boresight intersection
- DECLINATION - instantaneous declination of satellite-earth center vector from equatorial plane
- MIN BMWDTH - beamwidth along minor axis of beam cross section at -3 db (half-power) level
- MAX BMWDTH - beamwidth along major axis of beam cross section at -3 db (half-power) level
- ORIENTATION - orientation angle of beam about beam center
- ELEVATION - angle formed by vector RS and a plane tangent to earth at boresight intersection

The remainder of the printout gives the maximum and minimum beamwidth and a listing of the coordinates of the locus of intersection for each signal level.

Each set of input data is given a data set number. This number appears on the printout and the plot for each data set. This facilitates matching of plots with printout when more than one data set is run.

A modification of this program has recently been developed to plot the coverage of a multi-beam satellite. This new program computes the locus of intersection of a number of sets of input data as does the original. However, the modification plots all of the intersection loci on one set of axes so that uncovered areas and overlapped areas are immediately obvious.

The major changes to the original program are:

1. The plotter tape is opened and the axes are drawn before the main calculation begins.
2. The axes are scaled once at the beginning of the program rather than being scaled for each data set.
3. The computed coordinates are checked to see that they do not extend beyond the limits of the axes.
4. The plot origin is not reset for each data set.

IV. TYPICAL EXAMPLES

Figures 5-9 present the area coverage plots for input values shown in Table 1. For each case, 3, 5 and 10 dB level contours are plotted. The inputs represent a wide variety of cases--satellites positioned in circular, equatorial and geosynchronous orbits; satellites positioned in slightly inclined stationary orbits; and area coverage at small inclination angles.

Figure 10 shows the coverage provided by a 4-beam satellite positioned at 120°W longitude. All plots use the same set of axes. The input values for various beams are given in Table 2. All four beams are designed to provide complete coverage to the United States--beam 1 covers Hawaii, beam 2 covers Alaska, and beams 3 and 4 provide coverage to the other 48 states.

Table 1. Input Values for Coverage Plots shown in Figures 5-9

Input	Case I (Figure 5)	Case II (Figure 6)	Case III (Figure 7)	Case IV (Figure 8)	Case V (Figure 9)
Subsatellite Longitude	-115.00	-115.00	-115.00	-115.00	-115.00
Boresight Longitude	-157.00	-157.00	- 74.00	- 74.00	- 74.00
Boresight Latitude	21.30	21.30	40.75	40.75	40.75
Declination (in degrees)	0.00	0.00	0.00	1.00	0.00
Minor-axis Beamwidth (in degrees)	1.50	0.75	1.00	1.00	1.00
Major-axis Beamwidth (in degrees)	1.50	1.50	1.00	1.00	0.50
Orientation (in degrees)	0.00	- 25.00	0.00	0.00	40.00

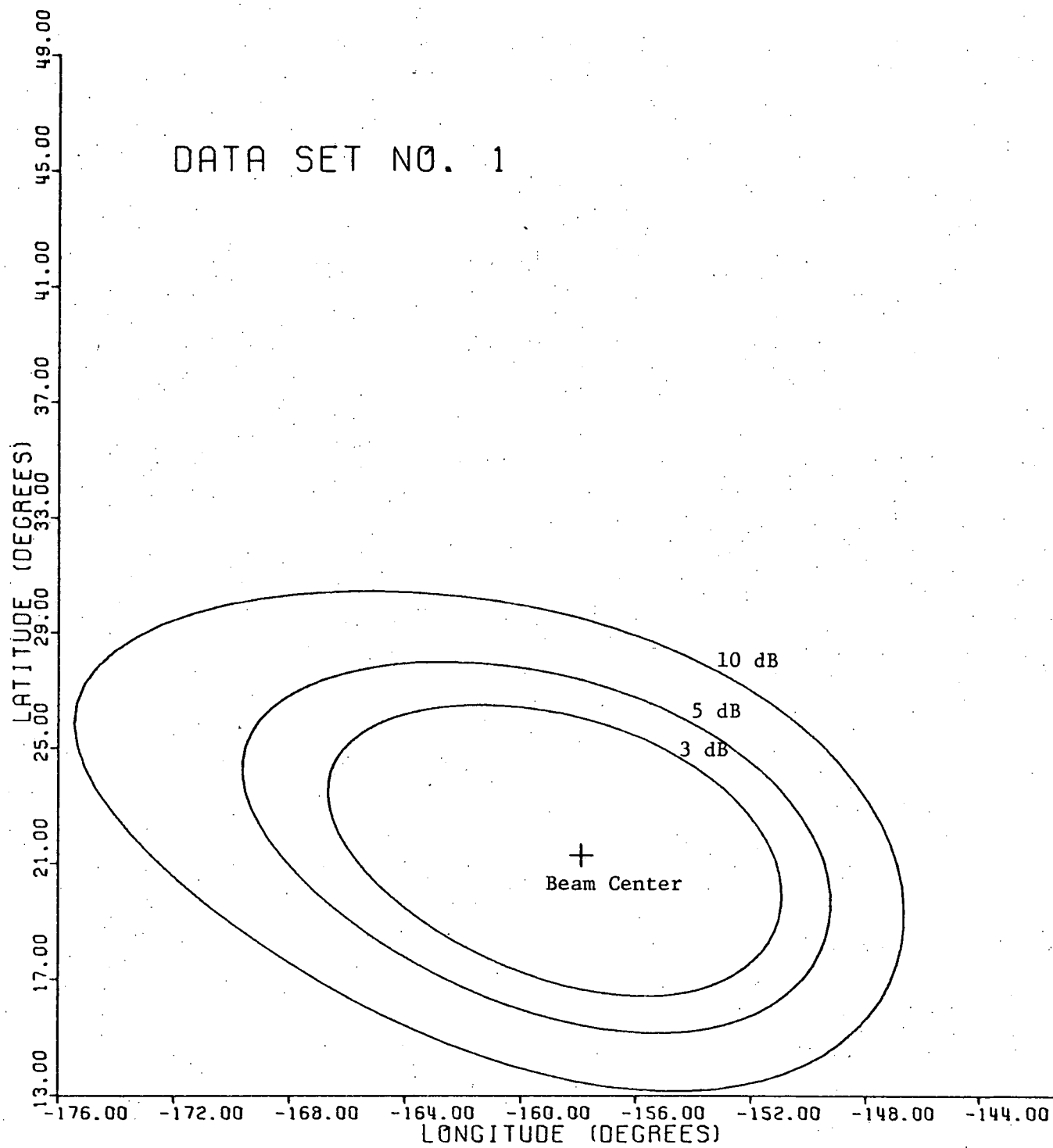


Figure 5

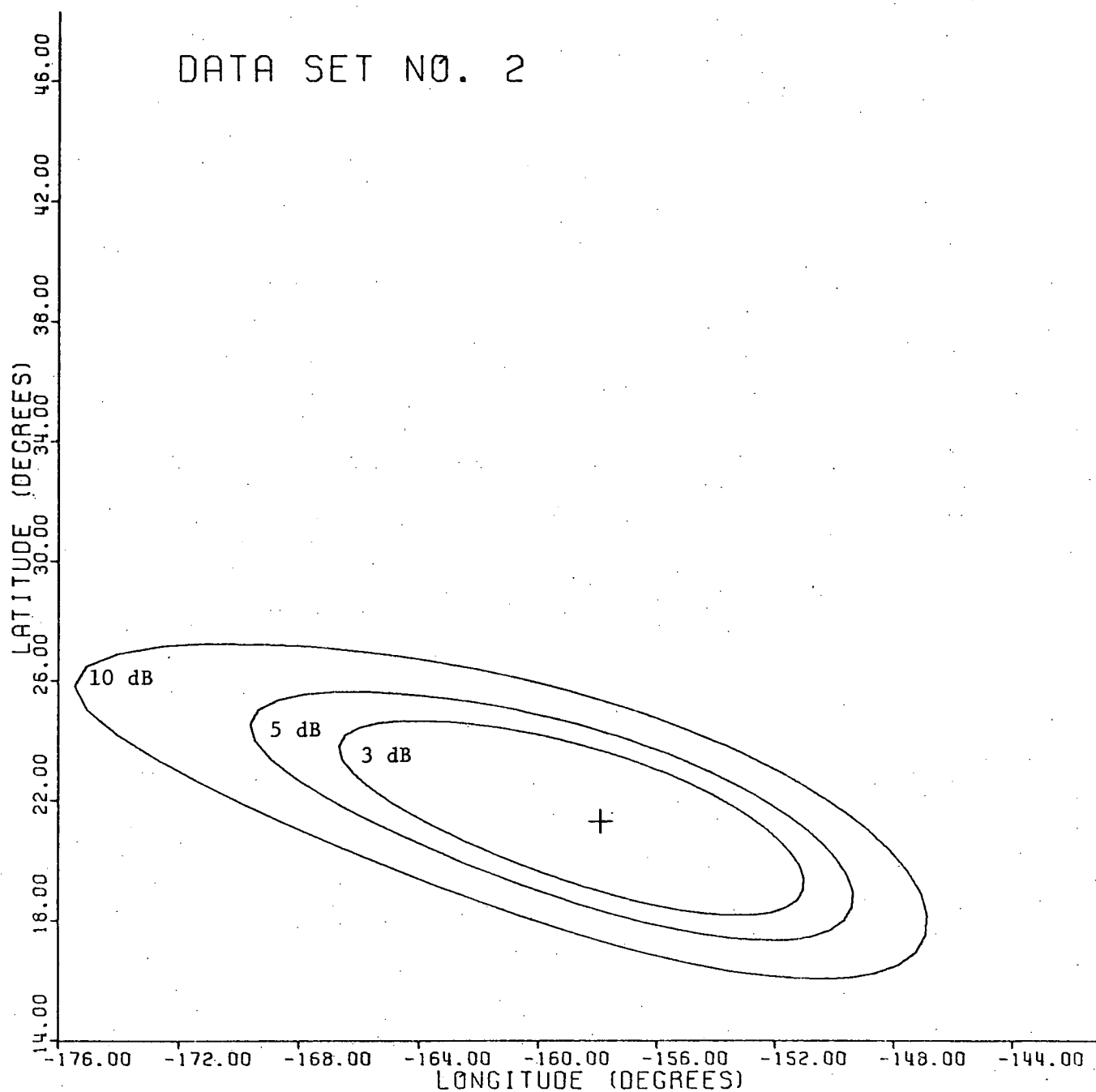


Figure 6

DATA SET NO. 3

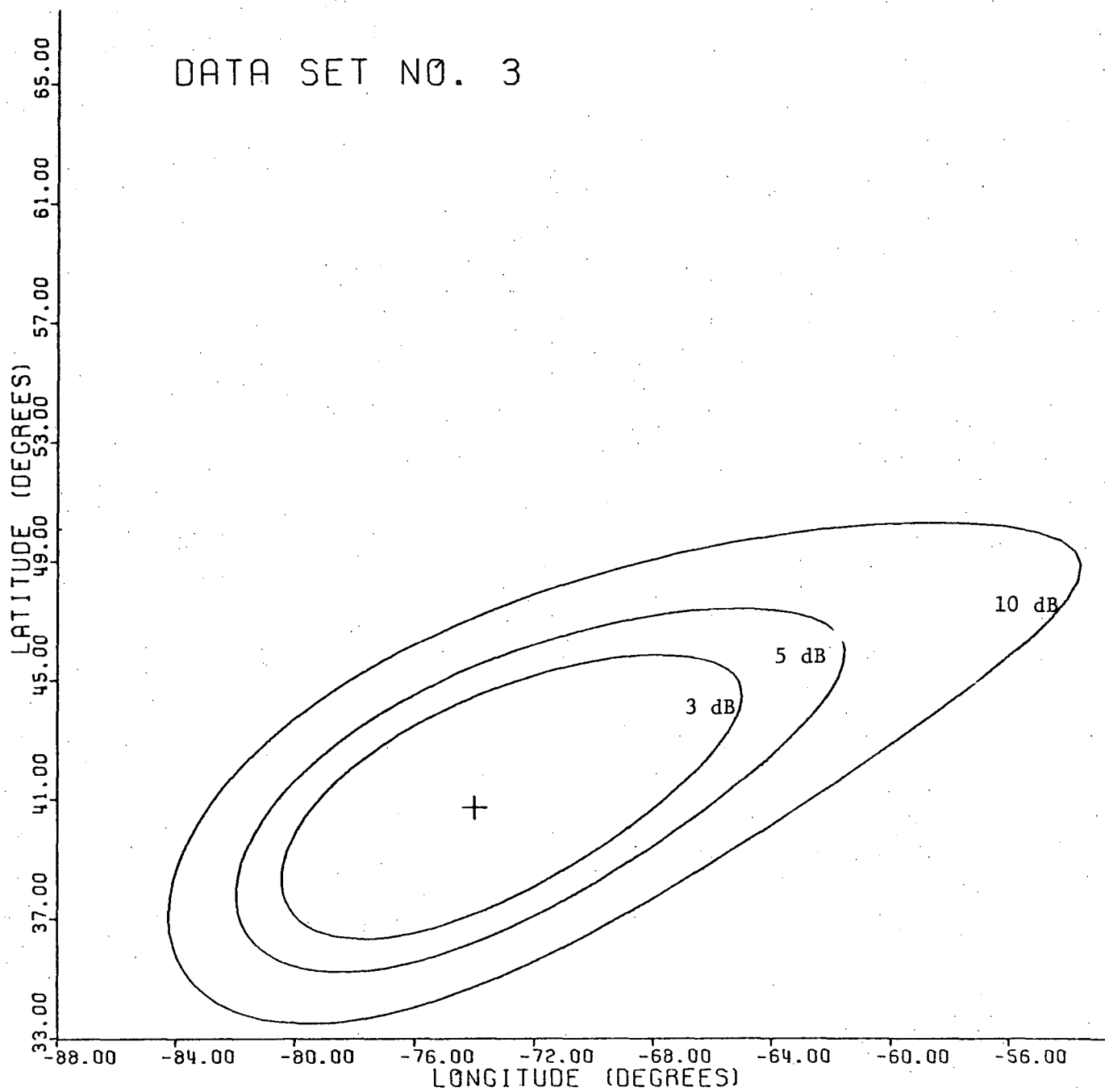


Figure 7

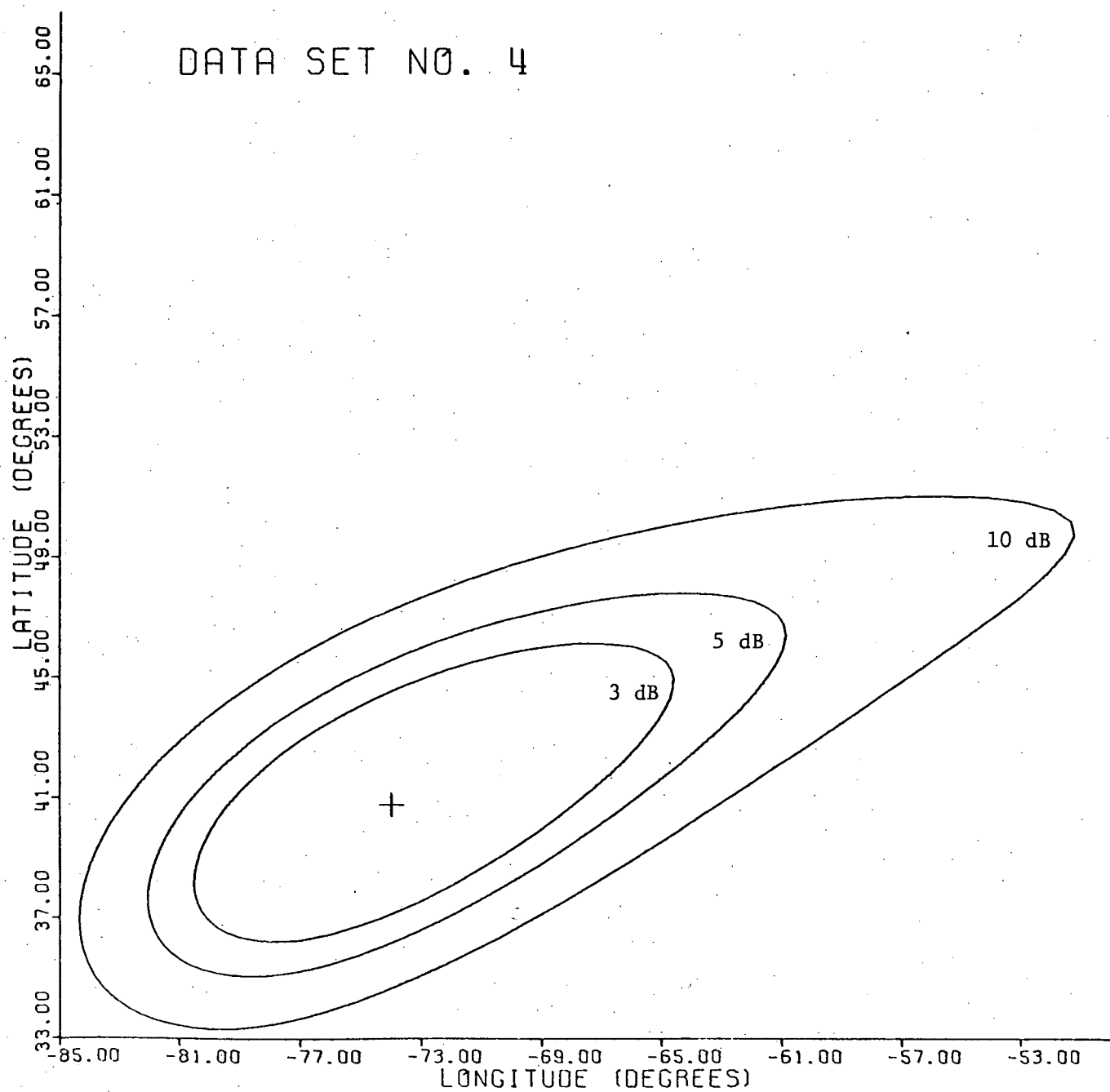


Figure 8

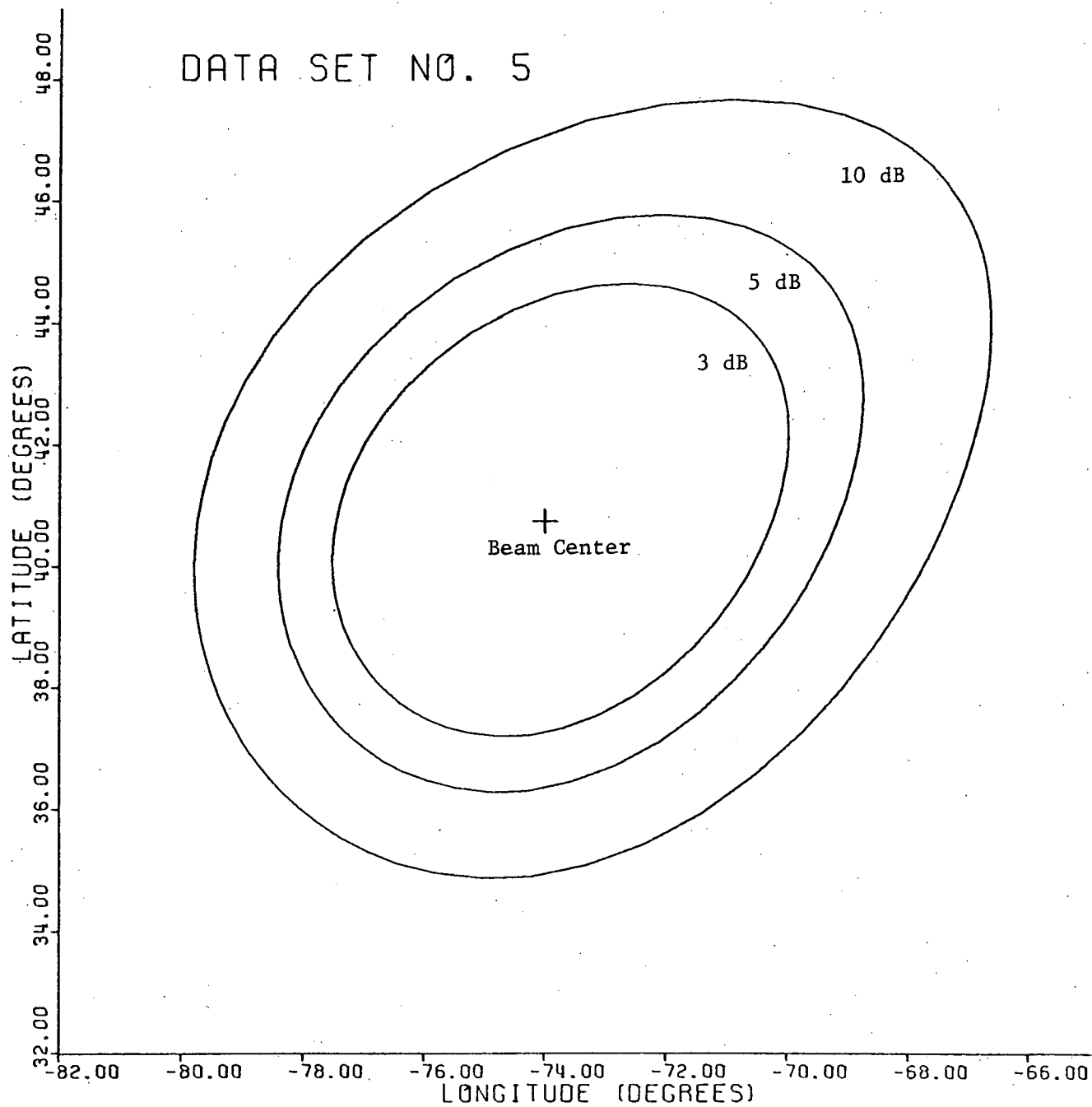


Figure 9

Table 2. Input Values for 4-Beam Coverage Plot Shown in Figure 10

Input	Hawaii	Alaska	Beam I for western and mountain states	Beam II for eastern and central states
Subsatellite Longitude	-120.00	-120.00	-120.00	-120.00
Boresight Longitude	-158.00	-145.00	-112.00	- 88.00
Boresight Latitude	21.00	63.00	37.00	36.00
Satellite Declination (in degrees)	0.00	0.00	0.00	0.00
Minor-axis Beamwidth (in degrees)	1.50	1.50	3.30	3.30
Major-axis Beamwidth (in degrees)	2.00	2.30	3.40	3.70
Orientation (in degrees)	135.00	110.00	0.00	0.00

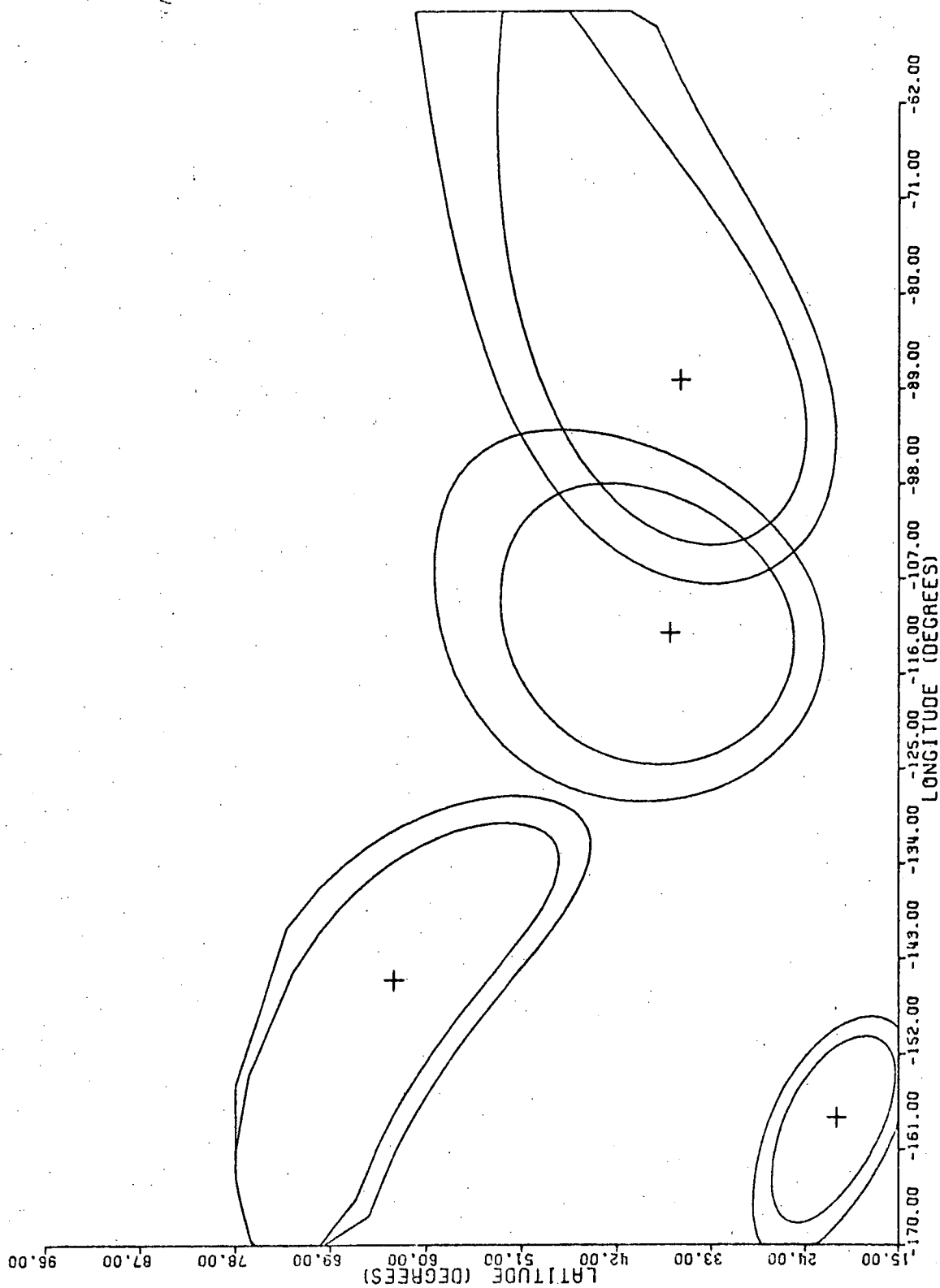


Figure 10. Four Beam Coverage of U.S. (see Table 2)

V. REFERENCES

1. S. L. Zolnay, "Earth Coverage ('Footprint') of a Satellite-Borne Antenna", Technical Note 1971-7, Lincoln Laboratory, Massachusetts Institute of Technology, Lexington, Massachusetts (February 5, 1971).
2. Theodore S. Saad, "Antennas" in Microwave Engineers Handbook (Vol. 2), Dedmam, Massachusetts: Artech House, Inc., p. 24.
3. W. Solfrey, "Earth Coverage Patterns with High Gain Antenna on Stationary Satellites", Memorandum RM-4894-NASA, The Rand Corporation, Santa Monica, California (1967).

APPENDIX A

PROGRAM LISTING

```
0001 IMPLICIT REAL*8(A-Z)
0002 REAL*8 DSIN,DCOS,DSQRT,DARSIN,DARCOS,DATAIN
0003 INTEGER*4 NSTEPS,ICT,I,N,NPLT,IBUF(1000),NP1,NP2,NDB,LDB
0004 INTEGER*4 J,J1,L,K
0005 INTEGER*4 FMT(4)/(' ','F7.3',' ','/
0006 INTEGER*4 DIGIT(10)/('1','2','3','4','5','6','7','8','9','10','/
0007 REAL*4 LGN(722),LAT(722),NL,XCT,YCT
0008 DIMENSION DB(10),DBS(8),RBS(8)
0009 DATA DBS/.1,.2,.5,.1,.1,.5,.3,.5,.10./
0010 DATA RBS/.18,.26,.4,.56,.7,.1,.1,.27,.1.7/
0011 DATA PI/3.14159265358979300/,RE/3.9603/,DIST/2.62604/
0012 N=0
0013 NPLT=0
0014 CONVTR=PI/180.
0015 UM=DARSIN(RE/DIST)
0016 CHK=81.3*CONVTR
0017 1 READ(5,500,END=1000)DLONSS,DLONCT,DLATCT,DINCR,DDELT
0018 500. FORMAT(5F9.3)
0019 READ(5,501)THETA1,BW1A,BW2A,L
0020 501. FORMAT(3F9.3,I2)
0021 FMT(2)=DIGIT(L)
0022 READ(5,FMT)(DB(I),I=1,L)
0023 NDB=0
0024 N=N+1
0025 WRITE(6,600)N,DLONSS,DLONCT,DLATCT,CDELT,BW2A,BW1A,THETA1
0026 600. FORMAT(/,'1 DATA SET NO. ',I2/,'4X',SUB_SAT_LONG =',F9.3/
1 4X,'BOR SIGHT LONG =',F9.3/,'4X',BOR_SIGHT_LAT =',F9.3/
2 4X,'DECLINATION =',F9.3/,'4X',MIN_BMWOTH',5X,'=',F9.3/
3 4X,'MAX BMWOTH',5X,'=',F9.3/,'4X',ORIENTATION =',F9.3/
C CONVERT FROM DEGREES TO RADIAN
0027 INCR=DINCR*CONVTR
0028 LONGCTR=(DLONCT-DLONSS)*CONVTR
0029 LATCTR=DLATCT*CONVTR
0030 DELT=DDELT*CONVTR
0031 BW1=BW1A*CONVTR/2.0
0032 BW2=BW2A*CONVTR/2.0
0033 THETA=THETA1*CONVTR
C CHECK FOR BORESIGHT LOCATION IN RANGE OF SATELLITE
0034 AL=DARCOS(DCOS(LONGCTR)*DCOS(LATCTR+DELT))
0035 IF(AL.LE.CHK)GO TO 21
0036 20 WRITE(6,400)
0037 400. FORMAT(1H0,'BORESIGHT LOCATION IS NOT IN RANGE OF SATELLITE.'/)
0038 GO TO 1
C COMPUTE VECTOR FROM SATELLITE TO BORESIGHT LOCATION
0039 21 RSX=RE*DCOS(LATCTR)*DSIN(LONGCTR)
0040 RSY=DIST*DCOS(DELT)-RE*DCOS(LATCTR)*DCOS(LONGCTR)
0041 RSZ=DIST*DSIN(DELT)+RE*DSIN(LATCTR)
0042 RSM=DSQRT(RSX**2+RSY**2+RSZ**2)
```

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0043 GAM=DARSIN(RE*DSIN(AL)/RSM)
0044 EL=((PI/2.0)-(AL+GAM))/CONVR
0045 WRITE(6,300) EL
0046 300 FORMAT(4X,'ELEVATION',6X,'=',F9.3)
0047 DENOM=DSQRT(RSX**2+RSY**2)
0048 PITCH=DARSIN(RSX/DENOM)
0049 ROLL=DATAN(RSZ/DENOM)
0050 CP=DCOS(PITCH)
0051 CR=DCOS(ROLL)
0052 SP=DSIN(PITCH)
0053 SR=DSIN(ROLL)
0054 MPLT=NPLT+1
0055 IF(INPLT.GT.1)GO TO 15
C FIRST PLOT, OPEN PLOTIAPE AND SET ORIGIN
0056 CALL PLOTS(IDUF,1000)
0057 CALL PLOT(1.0,1.0,23)
0058 GO TO 12
C NOT FIRST PLOT, SET ORIGIN
0059 15 CALL PLOT(1.0,1.0,-3)
0060 12 DO 31 K=1,L
0061 NOB=NDB+1
0062 LDB=L-K+1
C INTERPOLATE FOR RELATIVE BEAMWIDTH
0063 DO 8 J=1,8
0064 IF(DB(LDB)-DBS(J))6,7,8
0065 7 RBW=RBWS(J)
0066 GO TO 9
0067 8 CONTINUE
0068 6 J1=J-1
0069 RBW=(DB(LDB)-DBS(J1))*(RBWS(J)-RBWS(J1))/(DBS(J)-DBS(J1))
1
9 A=RSM*DTAN(BW1*RBW)
0070 B=RSM*UTAN(BW2*RBW)
0071 ALPHA=BW1A*RBW
0072 ALPHA2=BW2A*RBW
0073 NSTEPS=(360.0/DINCR)+1
0074 BMDTH=DALPHA*RBW
0075 DO 10 ICT=1,NSTEPS
0076 BETAN=(ICT-1)*INCR
0077 ANG=BETAN+THETA
0078 UN=1.0/USQRT((DCOS(BETAN)/A)**2+(DSIN(BETAN)/B)**2)
0079 C COMPUTE N-TH M VECTOR FROM SATELLITE TO LOCUS ON EARTH
0080 MNPX=RSM*CR*SP+UN*DCOS(ANG)*CP-UM*DSIN(ANG)*SR*SP
0081 MNPY=RSM*CR*CP+UN*DCOS(ANG)*SP-UM*DSIN(ANG)*SR*CP
0082 MNPZ=RSM*SR+UM*DSIN(ANG)*CR
0083 MNX=MNPX
0084 MNY=MNPY*DCOS(DELT)+MNPZ*DSIN(DELT)
0085 MNZ=MNPY*(-USIN(DELT))+MNPZ*DCOS(DELT)

```

```

0086 RN=DARCOS(MNVDSCRT(MNX**2+MNY**2+MNZ**2))
0087 IF(BN.GT.BM)GO TO 30
0088 CN=PI-DARSIN(DSIN(BN)*DIST/RE)
0089 DN=PI-(BN+CN)
0090 MNL=DSQRT(RE**2+DIST**2-2.*RE*DIST*DCOS(DN))
0091 DENOM=DSQRT(MNPX**2+MNPY**2)
0092 PITCHN=DARSIN(MNPX/DENOM)
0093 ROLLN=DAIAN(MNPZ/DENOM)
0094 REI=MNL*DCOS(ROLLN)*DSIN(PITCHN)
0095 REJ=DIST*DCOS(DELT)-MNL*DCOS(ROLLN)*DCOS(PITCHN)
0096 REK=MNL*DSIN(ROLLN)-DIST*DSIN(DELT)
0097 GO TO 40

C COMPUTE N-TH VECTOR FROM CENTER OF EARTH TO LOCUS
0098 REI=MNL*DCOS(ROLLN)*DSIN(PITCHN)
0099 REJ=DIST*DCOS(DELT)-MNL*DCOS(ROLLN)*DCOS(PITCHN)
0100 REK=MNL*DSIN(ROLLN)-DIST*DSIN(DELT)
0101 IF(MNX.LT.0.0)TAUN=-TAUN
0102 REI=RE*DCOS(BM)*DSIN(TAUN)
0103 REJ=RE*(-DCOS(DELT)*DSIN(BM)-DSIN(DELT)*DCOS(BM)*DCOS(TAUN))
0104 REK=RE*(-DSIN(DELT)*DSIN(BM)+DCOS(DELT)*DCOS(BM)*DCOS(TAUN))
0105 DEN=DSQRT(REI**2+REJ**2)
0106 COMPUTE LONGITUDE AND LATITUDE COORDINATES
0107 LAT(1CT)=SING(DATAN(REK/DEN)/CONVTR)
0108 LONG(1CT)=SING(DARSIN(REJ/DEN)/CONVTR+DLONSS)
0109 WRITE(6,100)DB(LC9),ALPH1,ALPH2
0110 100.FORMAT(1H-,3X,'AJ',F4.1,'DB LEVEL:',/4X,'MAX BMDIH=',F5.2/
0111 1 4X,'MIN BMDWH=',F5.2//
0112 2 5X,'LONGITUDE',7X,'LATITUDE',/5X,'(DEGREES)',6X,'(DEGREES)'
0113 3 /)
0114 00 80 I=1,NSTEPS
0115 80 WRITE(6,200) LONG(I),LAT(I)
0116 200.FORMAT(1H,4X,F9.3,6X,F9.3)
0117 IF(NDB.GT.1)GO TO 93
0118 C IF FIRST DB LEVEL PLOT AXES AND TITLES
0119 CALL SCALE(LGN,9.0,NSTEPS,1)
0120 CALL SCALE(LAT,9.0,NSTEPS,1)
0121 NP1=NSTEPS+1
0122 NP2=NSTEPS+2
0123 IF(LON(NP2)-LAT(NP2))90,91,92
0124 90 LONG(NP2)=LAT(NP2)
0125 GO TO 91
0126 92 LAT(NP2)=LGN(NP2)
0127 91 CALL AXIS(0.0,0.0,'LONGITUDE (DEGREES)',-19,9.0,0.0,LON(NP1),
0128 1 LCN(NP2))
0129 CALL AXIS(0.0,0.0,'LATITUDE (DEGREES)',18,9.0,0.0,LAT(NP1),
0130 2 LAT(NP2))
0131 SCFCT=LON(NP2)
0132 EVAL=LON(NP1)

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0124 FVLT=LAT(NP1)
0125 XCT=(SNGI(DLONCT)-LON(NP1))/LON(NP2)
0126 YCT=(SNGI(DLATCT)-LAT(NP1))/LAT(NP2)
0127 CALL SYMBOL(XCT,YCT,0.21,3,0.0,-1)
0128 CALL SYMBOL(1.0,8.0,0.21,'DATA SET NO. ',0.0,13)
0129 NI=FLOAT(N)
0130 CALL NUMBER(999.0,999.0,0.21,N1,0.0,-1)
0131 93 LON(NP2)=SCFCT
0132 LAT(NP2)=SCFCT
0133 LON(NP1)=FVLN
0134 LAT(NP1)=FVLT
      C PLOT COORDINATES OF LOCUS
0135 CALL LINE(LON,LAT,NSTEPS,1,0,0)
0136 31 CONTINUE
0137 CALL PLOT(14.0,-1.0,23)
0138 GO TO 1
0139 1000 IF(NPLT.LE.0) GO TO 1001
      C CLOSE PLOTTAPE
0140 CALL PLOT(0.0,0.0,999)
0141 1001 WRITE(6,700) NPLT
0142 700 FORMAT('NUMBER OF PLOTS PRODUCED =',I3)
0143 STOP
0144 END
```